

Modeling & Kinetics Studies of Doped Magnesium Borohydrides

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Abstract: $Mg(BH_4)_2$ is a potential solid state hydrogen storage material with high gravimetric hydrogen holding capacity. The effects of mechanical milling of $Mg(BH_4)_2$ with CaH_2 and CaH_2/NaH on its rate of hydrogen desorption were investigated at constant thermodynamic driving force. There is at least a two fold increase in the hydrogen desorption kinetics of $Mg(BH_4)_2$ resulting from the two additives. The rate of hydrogen release from the $Mg(BH_4)_2/CaH_2/NaH$ system is twice as fast as that of $Mg(BH_4)_2/CaH_2$. Modeling studies, based on a shrinking core model, showed that reaction at the phase boundary is the rate-limiting process in the hydrogen desorption from $Mg(BH_4)_2/CaH_2$ up to 70% of the reaction. In the $Mg(BH_4)_2/CaH_2/NaH$ systems, reaction at the phase boundary is the rate controlling process up to about 90% of the reaction.

Key Words: Magnesium borohydride; Plateau pressure; Opposing pressure; Kinetics; Modeling.

INTRODUCTION

The desire to have a clean atmosphere has led to an increased urge to develop alternative sources of energy. The greatest challenge with the use of hydrogen as a source of fuel is the unavailability of suitable storage mechanisms. For solid state hydrogen storage in automobiles, complex metal hydrides that are lightweight, low cost, and high in hydrogen density are potential candidates [1,2]. The use of Mg(BH₄)₂ as a potential storage material has been gaining popularity in recent times due to its high gravimetric hydrogen content of 14.9 wt% [3-11]. The hydrogen, however, cannot be easily harnessed due to thermodynamic and kinetic barriers. Studies have shown that in complete dehydrogenation, Mg(BH₄)₂ should produce MgB₂ and 4 moles of hydrogen gas, according to equation (1) [12,13].

$$Mg(BH_4)_2 \rightarrow MgB_2 + 4H_2$$
(1)

A popular way of improving the hydrogen storage properties of hydride compounds, first developed by

Reilly and Wiswall [14], is mixing/destabilizing with other additives. Vajo et al. [15,16] showed that addition of MgH₂ to LiBH₄ reduces its desorption temperature by changing the reaction pathway. The mixture also became reversible under moderate conditions. Similarly, a mixture of CaH₂ and LiBH₄ was predicted by Alapati et al. [17,18] to release 11.7 wt% of hydrogen, according to equation (2). They also calculated the enthalpy of the reaction to be 47 kJ/mol H₂.

$$LiBH_4 + CaH_2 \rightarrow 6LiH + CaB_6 + 10H_2$$
(2)

Studies showed that the system released hydrogen at a lower temperature than pure LiBH₄ [19-24]. Pinkerton and Meyer [21] reported that samples of $6LiBH_4 + CaH_2 +$ 0.25 TiCl₃, prepared by ball milling, released about 9.1 wt% of hydrogen during a TGA scan and that samples were successfully rehydrogenated under 83 bar H₂ and 400°C.

Severa et al. [8] found that it was possible to reversibly store about 11 wt% hydrogen in $Mg(BH_4)_2$. This was achieved under extreme conditions by direct hydrogenation of MgB_2 at a pressure of 900 bar and a temperature of 400°C. The addition of catalyst/additives has also been reported to improve the hydrogen storage properties of Mg(BH₄)₂ [25 - 28]. For instance, Yang et al. [26] reported the reduction of the onset temperature for hydrogen release to 150°C by the addition of LiH. It was also shown by Bardaji et al. [12] that a composite mixture of LiBH₄ and Mg(BH₄)₂ releases about 7 wt% of hydrogen at lower temperature than that of the individual borohydrides. A theoretical study by Ozolin et al. [29] using DFT calculations identified some reaction schemes that have the potential of reversibly storing hydrogen. Some of these reactions schemes that have been studied by our group are highlighted in equations (3)-(5).

$$5Mg(BH_4)_2 + Ca(BH_4)_2 \rightarrow CaB_{12}H_{12} + 5MgH_2 + 13H_2$$
 (3)

 $3Mg(BH_4)_2 + CaH_2 \rightarrow 3MgH_2 + CaB_6 + 10H_2$ (4)

 $3Mg(BH_4)_2 + CaH_2 + 3NaH \rightarrow 3NaMgH_3 + CaB_6 + 10H_2$ (5)

In previous studies, we determined the hydrogen properties of these systems [10]. We also found that the mixture of $Mg(BH_4)_2$ and $Ca(BH_4)_2$ releases hydrogen at a faster rate than either of the components [11].

In this present study, we present the kinetics and modeling studies of hydrogen desorption of systems in reaction schemes (4) and (5).

EXPERIMENTAL

CaH₂ and NaH were obtained from Sigma-Aldrich and were used without further treatment. Unsolvated Mg(BH₄)₂ was prepared from MgH₂ and triethylamine borane, as described by Chłopek et al. [9]. All sample preparations were carried out in an argon-filled Vacuum Atmospheres glove box with oxygen and moisture levels below 1 ppm. The sample mixtures were ball-milled for 10 h using a SPEX 8000D mixer/mill. PCT isotherms were determined for each sample using an Advanced Materials Corporation Gas Reaction Controller PCI unit. This unit was fully automated and was controlled by a Lab Viewbased software program. Kinetics measurements were done in an all stainless steel Sieverts apparatus. This apparatus is described in Fig. 1. It contained a back pressure regulator for controlling the pressure that was applied to the sample. Pressure transducers were used to monitor the pressure in the reservoirs and the sample reactor. Kinetics measurements were done at the same temperature and thermodynamic driving force. The thermodynamic driving force, denoted as the N-Value, is defined as the ratio of the mid plateau pressure, P_m, to the opposing pressure, P_{opp} (i.e., $N=P_m/P_{opp}$). The experiments were all carried out at 450 °C and N =10. Further details about the technique of constant pressure thermodynamic forces are published elsewhere [10, 11, 23, 24, 30, 31].



Fig 1: Schematic diagram of the apparatus used for kinetics measurements.

RESULTS & DISCUSSIONS

Desorption kinetics of the Mg(BH₄)₂/CaH₂ and Mg(BH₄)₂/CaH₂/NaH mixtures as well as that of the pure Mg(BH₄)₂ components were performed at 450 °C (Fig. 2). These measurements were carried out at a constant pressure thermodynamic driving force of N=10. In order to accomplish this, it was first necessary to determine a PCT isotherm for each sample. The PCT isotherms of Mg(BH₄)₂ and the mixtures at 450 °C have been reported [10,30]. The opposing pressures determined for the mixtures from the isotherms are shown in Table 1.

Table 1: Plateau pressures, opposing pressures, & Reaction times to reach 90 %, T₉₀ completion for borohydride systems at N=10 and 450°C.

System	Plateau pressure (atm)	Opposing pressure (atm)	T90 (min)
Mg(BH ₄) ₂	62.0	6.2	12.0
$Mg(BH_4)_2/Ca(BH_4)_2$	64.0	6.4	4.0
Mg(BH ₄) ₂ /CaH ₂	57.0	5.7	5.0
Mg(BH ₄) ₂ /CaH ₂ /NaH	56.0	5.6	2.5

All of the reactions are faster than that of pure $Mg(BH_4)_2$. All of the reactions except $Mg(BH_4)_2$, reached 90% completion on or before 5 minutes. Table 1 shows the time taken for the hydrogen desorption reactions to reach 90% completion (T₉₀). It takes about 12 min for the pure $Mg(BH_4)_2$ to reach T₉₀, while the mixtures take between 2.5 - 4.0 mins to reach 90% completion. All the mixtures have also been reported to have higher desorption temperatures than the pure $Mg(BH_4)_2$, except the $Mg(BH_4)_2/CaH_2/NaH$ mixture [30].

Modeling studies were done to determine the process controlling the rates of hydrogen desorption from the systems. A set of equations used by Smith and Goudy [31] in modeling the LaNi_{5-x}Co_x hydride system were used. The models were used to determine whether the hydrogen desorption process is controlled by a reaction occurring at phase boundary or hydrogen diffusion.

$$\frac{t}{\tau} = 1 - (1 - X_B)^{1/3} \tag{6}$$

Where

$$\tau = \frac{\rho_B R}{bk_S C_{Ag}}$$

$$\frac{t}{\tau} = 1 - 3(1 - X_B)^{2/3} + 2(1 - X_B) \quad (7)$$

Where

$$\tau = \frac{\rho_B R^2}{6b D_e C_{Ag}}$$

The various terms in the equations are defined as follows: t = time at a specific point in the reaction; $X_B =$ fraction of the material reacted; R = initial radius of the sample particles; b = stoichiometric coefficient of the material; $C_{Ag} =$ the gas phase concentration of the reactant; $D_e =$ the effective diffusivity of the hydrogen atoms in the material; $\rho_B =$ the density of the material; and $k_S =$ a rate constant. In the modeling studies, the experimental kinetics data of the systems were statistically fitted with theoretically generated data based on equations (6) and (7).



Fig 2. Combined plots of reacted fraction versus time for Mg(BH₄)₂, Mg(BH₄)₂/Ca(BH₄)₂, Mg(BH₄)₂/CaH₂ and Mg(BH₄)₂/CaH₂/NaH mixtures at 450°C and N = 10

Values of τ were selected that minimized the difference between the experimental and theoretical curves. The parameters (R, b, De, ρ B, and ks) were not used to determine τ in the equations and we don't have their values. Tau (τ) is essentially a fitting parameter. The values of τ for each reaction were determined statistically by minimizing the standard deviation between the experimental and theoretical curves. Equation (6) corresponds to a situation in which the rate is controlled

by diffusion, while equation (7) is that of a process where the rate is controlled by reaction at the phase boundary.



Fig 3: The shrinking core model.

Equations (6) and (7) are based on a shrinking core model in which desorption begins from a fully hydrided sphere. As hydrogen desorbs from the particle, an outer layer of dehydrided material begins to cover the sphere. The outer dehydrided layer grows as hydrogen desorption continues and the inner sphere shrinks. A phase boundary separates the outer and inner spheres. A schematic of this shrinking core model is shown in Fig. 3. Hydrogen desorption occurs at the phase boundary and hydrogen atoms diffuse through the outer dehydrided layer. The two processes occur simultaneously throughout the entire desorption process. The kinetics may be limited by the rate of reaction at the phase boundary or by the rate of hydrogen diffusion through the outer dehydrided layer, depending on which is slower.

The plot in Fig. 4 for $Mg(BH_4)_2/CaH_2$ shows that the phase boundary controlled model fits the experimental curve up to 70% of the reaction, while the diffusion controlled model fits between 75 and 85%. Above that region, none of the two models fits. Therefore, the system rate determining step changes during the course of the reaction. The results correspond to those reported earlier for the $Mg(BH_4)_2/Ca(BH_4)_2$ system [11]. The CaH_2 changed the rate determining process of the mixture from that of pure $Mg(BH_4)_2$ controlled by the diffusion process [11].



The modeling curve of the Mg(BH₄)₂/CaH₂/NaH mixture is shown in Fig. 5. Model fitting for the Mg(BH₄)₂/CaH₂/NaH mixture shows a good fit of the phase boundary controlled model with the experimental up to about 90% of the reaction. The diffusion controlled model does not fit at all for this process. Therefore, the rate limiting process in the dehydrogenation of Mg(BH₄)₂/CaH₂/NaH system is a reaction at the phase boundary. It can be seen that the mixture containing NaH released hydrogen at the fastest rate of any system under study. It may be that the Na+ enhances the rate of hydrogen diffusion in the system, thereby resulting in an increase in the overall reaction kinetics. The high desorption temperature of Mg(BH₄)₂/CaH₂/NaH, the highest of the three mixtures involving Mg(BH₄)₂, can be attributed to the high reactivity of the Na in the system [30].



CONCLUSION

The studies have shown that the rate of hydrogen desorption from $Mg(BH_4)_2$ can be increased by destabilization. The mechanical alloying of $Mg(BH_4)_2$ with CaH₂ and CaH₂/NaH improved the rate of hydrogen desorption, with the ternary mixture having the fastest kinetics. Modeling studies also show that the rate of hydrogen desorption from $Mg(BH_4)_2/CaH_2$ is controlled by reaction at the phase boundary in first 75% of the reaction, and changed to diffusion in 75-85% of the reaction. Furthermore, hydrogen desorption from $Mg(BH_4)_2/CaH_2/NaH$ is controlled by the reaction at the phase boundary up to 90% of the reaction based on the shrinking core model.

ACKNOWLEDGMENTS

This research was financially supported by the U.S. Department of Energy Grant Number DE-FC36-06GO86046 and the U.S. Department of Transportation Grant Number DTOS59-07-G-00056. The authors thank Dr. Andrew Goudy for providing the instrumentation used in this research.

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